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Skillful operators of defectoscopes. Put' i put.khoz. 6 no.11:35 '62. (MIRA 16:1)
(Railroads—Maintenance and repair)

VAGAYTSEV, V.I., tekhnik po defektoskopii (Chita)

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USSR / Virology. Human and Animal Viruses E-2

Abs Jour: Ref Zhur - Biol., No 6, 1958, 23955

Author : Vagazhanova, V. A.
Inst : Not given
Title : Interaction of Tumors and Viruses.

Orig Pub: Vopr. virusologii, 1957, No 3, 179-181

Abstract: When a mixture of Erlich ascitic carcinoma with viruses of tick encephalitis, encephalomyelitis, encephalomyocarditis, herpes, chick-pest and fixated rabies virus are administered to mice intracerebrally, the percentage of mouse deaths after a two-hour contact was higher than on administration of these viruses and ascitic carcinoma separately. In intraperitoneal administration of the enumerated viruses, as well as influenza and ectromelia viruses, the percentage of mouse

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USSR / Virology. Human and Animal Viruses E-2

Abs Jour: Ref Zhur - Biol., No 6, 1958, 23955

Abstract: deaths after a two hour contact differed but little from the control.

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L 43995-66 EWT(1) GW

ACC NR: AT6021504 (N) SOURCE CODE: UR/2531/66/000/187/0003/0012

AUTHOR: Vager, B. G.; Zilitinkevich, S. S.

ORG: none

21
B+1

TITLE: Method of calculating the height of the lower boundary of clouds based on numerical forecasting data

SOURCE: Leningrad. Glavnaya geofizicheskaya observatoriya. Trudy, no. 187, 1966. Fizika pogranichnogo sloya atmosfery (Physics of the atmospheric boundary layer), 3-12

TOPIC TAGS: atmospheric cloud, cloud cover, cloud level, WEATHER FORECASTING

ABSTRACT: An attempt is made to establish a functional relationship between the height of the lower boundary of the cloud cover and parameters the values of which lend themselves to numerical forecasting. In the mathematical description of the method, the input equations, boundary conditions, and integration of the input equations and additional simplifications which are performed on an electronic computer are cited. Several specific examples, the starting material for which were experimental data obtained from an investigation of the lower cloud cover during the fall of 1962 in the region of Dnepropetrovsk were examined in order to compare the calculated values of the height of the lower boundary of clouds with the observed

Card 1/2

L 43995-66

ACC NR: AT6021504

values. Their mean square deviation amounted to 149 m. Orig. art. has: 2 tables and 39 formulas.

SUB CODE: 04/ SUBM DATE: none/ ORIG REF: 016/ OTH REF: 002

Card 2/2 ULR

L 08153-67 EWT(1) GW

ACC NR: AT6021506 (N) SOURCE CODE: UR/2531/66/000/187/0044/0053

AUTHOR: Vager, B. G.; Tseytin, G. Kh.

27
25
B+1

ORG: none

TITLE: Structure of the atmospheric boundary layer under stationary conditions (nonlinear problem)

SOURCE: Leningrad. Glavnaya geofizicheskaya observatoriya. Trudy, no. 187, 1966. Fizika pogranichnogo sloya atmosfery (Physics of the atmospheric boundary layer), 44-53

TOPIC TAGS: atmospheric boundary layer, atmospheric turbulence, turbulent diffusion

ABSTRACT: A scheme is presented for computing some meteorological

structure of the atmospheric boundary layer under stationary conditions (nonlinear problem). IN: Glavnaya geofizicheskaya observatoriya. Fizika pogranichnogo sloya atmosfery (Physics of the surface boundary layer of the atmosphere), 1966, 44-53. (ITS: Trudy, no. 187, 1966).

A scheme is presented for computing some meteorological characteristics of the boundary layer of the atmosphere for various states of thermal stability, with turbulent energy diffusion taken into account. Since diffusion of turbulent energy can be neglected in the special case of neutral stratification, this method can be reduced to a numerical scheme for computation.

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ACC NR: AT6021506

The problem reduces to solving the following system of equations: equations of motion under horizontally homogeneous conditions:

$$\left.\begin{aligned} &\frac{d}{dz} k(z) \frac{du}{dz} + 2\omega_z v(z) = 0 \\ &\frac{d}{dz} k(z) \frac{dv}{dz} - 2\omega_z [u(z) - V_g] = 0 \end{aligned}\right\} \tag{1}$$

the equation of the influx of heat

$$\alpha k(z)\left[\frac{dT}{dz} + \gamma_p\right] = -\frac{P_0}{c_p \rho} - \frac{R(z) - R(0)}{c_p \rho}, \tag{2}$$

and the equations of turbulent energy balance

$$k(z)\left[\left(\frac{du}{dz}\right)^2 + \left(\frac{dv}{dz}\right)^2\right] - \frac{g}{T} \alpha k(z)\left[\frac{dT}{dz} + \gamma_p\right] - c_0 \frac{b^2(z)}{k(z)} + a_1 \frac{d}{dz} k(z) \frac{db(z)}{dz} = 0, \tag{3}$$

$$k(z) = l(z)\sqrt{b(z)}. \tag{4}$$

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The expression for the scale of turbulence $l(z)$ (according to D. L. Laykhtman and S. S. Zilitinkevich) is

$$l(z) = -2c_0^{\frac{1}{4}} \times \frac{F(z)}{\frac{dF(z)}{dz}}, \tag{5}$$

$$F(z) = \left(\frac{du}{dz}\right)^2 + \left(\frac{dv}{dz}\right)^2 - \frac{\alpha g}{T}\left(\frac{dT}{dz} + \gamma_p\right). \tag{6}$$

The following notation is adopted in equations (1)—(6): $u(z)$, $v(z)$ are the horizontal components of the wind velocity (the x-axis is directed along the isobar); $k(z)$ is the turbulence factor; v_g is the velocity of the geostrophic wind; $T(z)$ is the absolute air temperature; γ_p is the equilibrium temperature gradient; P_0 is the value of the turbulent heat flux at ground level; $R(z)$ is the radiant heat flux; $b(z)$ is the energy of turbulent pulsations; α is the ratio of the turbulence factor for heat to the turbulence factor for momentum; and c_0 and α_1 are constants. The remaining notation is standard. In this formulation of the problem, it is considered that the values of the radiation for $R(z)$ and turbulent flux near the ground P_0 are given. Thus, the system is closed with six equations (1—5) available for six unknowns: $u(z)$, $v(z)$, $k(z)$, $l(z)$, $b(z)$, and $T(z)$.

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The boundary conditions are as follows:

$$u(z)=v(z)=0 \text{ when } z=z_0$$

$$u(z) \underset{z\to\infty}{\rightarrow} V_g, \quad v(z) \underset{z\to\infty}{\rightarrow} 0, \qquad (7), (8)$$

$$k(z)\big|_{z=z_0}=\varkappa v_* z_0, \qquad (9)$$

where V_* is the dynamic velocity, and:

$$v_*^2=k(z)\sqrt{\left(\frac{du}{dz}\right)^2+\left(\frac{dv}{dz}\right)^2}\Bigg|_{z=z_0}, \qquad (10)$$

$$k(z)\frac{db(z)}{dz}\Bigg|_{z=z_0}=0, \qquad (11)$$

$$b(z) \underset{z\to\infty}{\rightarrow} 0, \qquad (12)$$

z_0 is the surface roughness parameter. The boundary condition (11) means that turbulent energy does not penetrate the underlying surface.

A scheme for solving the problem is given for the general case. First, the dimensionless height and the desired functions are introduced by the formulas:

$$\eta=V_g\int_{z_0}^{z}\frac{dz}{k(z)}=\frac{2\omega_z}{V_g}\int_{z_0}^{z}\frac{dz}{\beta(z)}, \qquad (13)$$

$$\beta(z)=\frac{2\omega_z}{V_g^2}k(z), \qquad (14)$$

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$$u_0(\eta) = \frac{u(\eta)}{V_g}, \quad v_0(\eta) = \frac{v(\eta)}{V_g} \tag{15}$$

$$\Phi(\eta) = \frac{c_0^{\frac{1}{2}}}{V_g^{\frac{1}{2}}} b(\eta). \tag{16}$$

Then, instead of equations (1), (3), and the boundary conditions (7), (8), (11), and (12), we get

$$\frac{d^2G(\eta)}{d\eta^2} - i\beta(\eta)G(\eta) = 0, \tag{17}$$

$$\frac{\varepsilon d^2\Phi(\eta)}{d\eta^2} - \Phi^3(\eta) + E(\eta) = 0, \tag{18}$$

$$G(\eta)\big|_{\eta=0} = 1, \tag{19}$$

$$G(\eta) \underset{\eta\to\infty}{\longrightarrow} 0, \tag{20}$$

$$\Phi(\eta) \underset{\eta\to\infty}{\longrightarrow} 0, \tag{21}$$

$$\left.\frac{d\Phi(\eta)}{d\eta}\right|_{\eta=0} = 0, \tag{22}$$

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where

$$\bar{G}(\eta) = 1 - u_0(\eta) - iv_0(\eta), \tag{23}$$

$$\mathrm{E}(\eta) = \left(\frac{du_0}{d\eta}\right)^2 + \left(\frac{dv_0}{d\eta}\right)^2 - s_1\beta^2(\eta)\left[\frac{dT}{dz} + \gamma_p\right] = \left(\frac{du_0}{d\eta}\right)^2 + \left(\frac{dv_0}{d\eta}\right)^2 + s_2\beta(\eta)P(z), \tag{24}$$

$$P(z) = -\alpha c_p \rho k(z)\left[\frac{dT}{dz} + \gamma_p\right], \tag{25}$$

$$s = \frac{a_1}{\sqrt{c_0}}, \tag{26}$$

$$s_1 = \frac{ag}{4\omega_z^2 T}, \tag{27}$$

$$s_2 = \frac{g}{2\omega_z c_p \rho T V_g^2}. \tag{28}$$

On the basis of (4), (5), (9), and (10), we find that

$$\beta(\eta) = m_0 \sqrt{\mathrm{E}(\eta)}\, e^{s\int_0 \sqrt{\Phi(\eta)}\, d\eta} \tag{29}$$

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where

$$m_0 = \frac{2\omega_z \varkappa z_0}{v_* \sqrt{1 + \frac{\varkappa z_0}{L}}}, \quad m_0 \approx \frac{2\omega_z \varkappa z_0}{v_*}, \qquad (30)$$

for $z_0 \ll L$, where $L = \frac{v_*}{\frac{g}{T} \cdot \frac{P_0}{c_p \rho}}$ is the height of the surface boundary sublayer, according to Obukhov and Monin. If stratification is neutral, when $L = \infty$, (30) becomes exact. When dT/dz or $P(z)$ is given for the case of an atmosphere which is not in a state of equilibrium, the system of equations, in dimensionless form, contains only the two parameters m_0 and s_1 (or s_2), and universal constants.

When the state of the atmosphere is neutral ($P(z) \equiv 0$), the system depends on only one parameter m_0 which can be expressed by the Rossby parameter

$$Ro = \frac{V_g}{2\omega_z z_0}. \qquad (31)$$

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Thus, the scheme for solving the system can be written, in the general case, as follows:

1) An approximate profile of the turbulence factor $\beta(\eta)$ is given;
2) The equation of motion (17) is solved by the selected $\beta(\eta)$ with boundary conditions (19)—(20);
3) The profile $E(\eta)$ is calculated by formula (24) with s_1 (or s_2) given and the profile dT/dz or $P(z)$;
4) The profile $\phi(\eta)$ is determined by formula (18), making use of $E(\eta)$ and boundary conditions (21)—(22);
5) A new profile $\beta(\eta)$ is determined by formula (29), using the given profile m_0 and profiles $\phi(\eta)$ and $E(\eta)$.

If the new profile differs noticeably from the preceding one, this procedure is repeated with the new profile, starting with step 2).

A simplified numerical method of computation is given for the case of neutral stratification (without taking turbulent-energy diffusion into consideration). In this case, equation (18) takes the form

$$E(\eta)-\Phi^2(\eta)=0, \tag{32}$$

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where

$$E(\eta)=\left(\frac{du_0}{d\eta}\right)^2+\left(\frac{dv_0}{d\eta}\right)^2. \tag{33}$$

Thus, equation (29) is replaced by

$$\beta(\eta)=m_0\sqrt{E(\eta)}\,e^{\int_0 E(\eta)^{\frac{1}{4}}d\eta} \tag{34}$$

Reducing the linear boundary problem to Cauchy problems, one can seek the desired function $\Theta(\eta)$ in the form

$$\Theta(\eta)=\Theta_1(\eta)-\frac{\Theta_1(\eta_H)}{\Theta_2(\eta_H)}\Theta_2(\eta), \tag{35}$$

where $\Theta_1(\eta)$ and $\Theta_2(\eta)$ are solutions of equation (17) with the boundary conditions

$$\Theta_1(\eta)\big|_{\eta=0}=1,\quad \frac{d\Theta_1(\eta)}{d\eta}\bigg|_{\eta=0}=0, \tag{36}$$

$$\Theta_2(\eta)\big|_{\eta=0}=0,\quad \frac{d\Theta_2(\eta)}{d\eta}\bigg|_{\eta=0}=1, \tag{37}$$

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and η_H is a sufficiently great height. Then

$$\left.\begin{aligned} Q_1(\eta) &= A(\eta) + iB(\eta) \\ Q_2(\eta) &= C(\eta) + iD(\eta) \end{aligned}\right\} \quad (38)$$

Then, we get instead of (17), (36), and (37):

$$\left.\begin{aligned} \frac{d^2A(\eta)}{d\eta^2} &= -\beta(\eta)B(\eta) \\ \frac{d^2B(\eta)}{d\eta^2} &= \beta(\eta)A(\eta) \\ \frac{d^2C(\eta)}{d\eta^2} &= -\beta(\eta)D(\eta) \\ \frac{d^2D(\eta)}{d\eta^2} &= \beta(\eta)C(\eta) \end{aligned}\right\} \quad (39)$$

$$\left.\begin{aligned} & A(\eta)\big|_{\eta=0} = 1, \quad B(\eta)\big|_{\eta=0} = 0 \\ & \frac{dA(\eta)}{d\eta}\Big|_{\eta=0} = 0, \quad \frac{dB(\eta)}{d\eta}\Big|_{\eta=0} = 0 \\ & C(\eta)\big|_{\eta=0} = 0, \quad D(\eta)\big|_{\eta=0} = 0 \\ & \frac{dC(\eta)}{d\eta}\Big|_{\eta=0} = 1, \quad \frac{dD(\eta)}{d\eta}\Big|_{\eta=0} = 0 \end{aligned}\right\} \quad (40)$$

The wind velocity components $u_0(\eta)$ and $v_0(\eta)$ are expressed

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by the formulas

$$\left.\begin{aligned} u_0(\eta) &= 1 - A(\eta) + L(\eta_{II})C(\eta) - \overline{L}(\eta_{II})D(\eta) \\ v_0(\eta) &= -B(\eta) + L(\eta_{II})D(\eta) + \overline{L}(\eta_{II})C(\eta) \end{aligned}\right\} \quad (41)$$

where

$$\left.\begin{aligned} L(\eta_{II}) &= \frac{A(\eta_{II})C(\eta_{II}) + B(\eta_{II})D(\eta_{II})}{C(\eta_{II})^2 + D(\eta_{II})^2} \\ \overline{L}(\eta_{II}) &= \frac{B(\eta_{II})C(\eta_{II}) - A(\eta_{II})D(\eta_{II})}{C(\eta_{II})^2 + D(\eta_{II})^2} \end{aligned}\right\} \quad (42)$$

The Adams method was used for numerical integration of the system (39)—(40) with modified coefficients in which differences up to the sixth order inclusive were taken into account. This permitted attaining quite high accuracy in determining not only the velocity components, but their derivatives which determine the vertical profiles of characteristics of turbulence $k(z)$, $b(z)$, and $l(z)$ with a comparatively small number of iterations (several tens). Applying the Adams method to system (39),

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$$\left.\begin{aligned} A'_{j+1} &= A'_j - hW_1(\beta_j A_j) \\ B'_{j+1} &= B'_j + hW_1(\beta_j A_j) \\ A_{j+1} &= A_j + hA'_j - h^2W_2(\beta_j B_j) \\ B_{j+1} &= B_j + hB'_j + h^2W_2(\beta_j A_j) \end{aligned}\right\} \quad (43)$$

and similar formulas for C, D, C', and D'. The following notation is used here:

$$\left.\begin{aligned} W_1(f_j) &= \frac{1}{60\,480}[198\,721 f_j - 447\,288 f_{j-1} + 705\,549 f_{j-2} - \\ &\quad - 688\,256 f_{j-3} + 407\,139 f_{j-4} - 134\,472 f_{j-5} + 19\,087 f_{j-6}] \\ W_2(f_j) &= \frac{1}{120\,960}[139\,849 f_j - 243\,594 f_{j-1} + 369\,399 f_{j-2} - \\ &\quad - 354\,188 f_{j-3} + 207\,495 f_{j-4} - 68\,106 f_{j-5} + 9625 f_{j-6}] \end{aligned}\right\}. \quad (44)$$

In order to determine the initial six values of the desired functions, it is assumed that the forces of turbulent friction noticeably overlap the effect of the Coriolis force in the surface boundary sublayer of the air, and the latter can be taken into consideration approximately in the layer $0 \leq \eta \leq 6h$, and making use of (17), (36)—(37):

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$$\left.\begin{aligned} Q_1(\eta) &\approx 1+i\int_0^\eta \beta(\xi)(\eta-\xi)\,d\xi \\ Q_2(\eta) &\approx \eta+i\int_0^\eta \beta(\xi)(\eta-\xi)\,\xi\,d\xi \end{aligned}\right\} \quad (45)$$

Representing the function $\beta(\eta)$ by the Lagrange interpolation formula for j ($j \leq 6$) of equispaced net points, the following formulas are obtained for computing the first seven ($j = 0, 1, \ldots, 6$) initial points:

$$\left.\begin{aligned} &A_j=1, \quad A_j'=0 \\ &B_j=h^2(\bar{\beta}\,\bar{b}_j), \quad B_j'=h(\bar{\beta}\,\bar{b}_j) \\ &C_j=hj, \quad C_j'=1 \\ &D_j=h^3(\bar{\beta}\,\bar{d}_j), \quad D_j'=h^2(\bar{\beta}\,\bar{d}_j) \end{aligned}\right\} \quad (46)$$

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where $\vec{\beta}$ is the column vector

$$\vec{\beta} = \begin{bmatrix} \beta_0 \\ \beta_1 \\ \beta_2 \\ \beta_3 \\ \beta_4 \\ \beta_5 \\ \beta_6 \end{bmatrix}, \tag{A}$$

and b_j, b_j', $\vec{d}_j$, $\vec{d}_j'$ are the j-th rows of matrices $\vec{B}$, $\vec{B}'$, $\vec{D}$, and $\vec{D}'$.

After computing the first seven points by formulas (46), further computations are carried out with formulas (43). After taking a sufficient number of steps and computing the values of the functions L and $\bar{L}$ by formulas (42) for the last step $j = N$ ($\eta_H = Nh$), the values of the speeds $u_0(\eta)$, $v_0(\eta)$, and their derivatives are found at points η_j ($j = 0, 1, \ldots, N$) by formulas (41).

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$$B = \begin{Vmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \frac{1}{3} & \frac{1}{6} & 0 & 0 & 0 & 0 & 0 \\ \frac{2}{3} & \frac{4}{3} & 0 & 0 & 0 & 0 & 0 \\ \frac{39}{40} & \frac{27}{10} & \frac{27}{40} & \frac{3}{20} & 0 & 0 & 0 \\ \frac{56}{45} & \frac{64}{15} & \frac{16}{15} & \frac{64}{45} & 0 & 0 & 0 \\ \frac{1525}{1008} & \frac{11\,875}{2016} & \frac{625}{504} & \frac{3125}{1008} & \frac{625}{1008} & \frac{275}{2016} & 0 \\ \frac{123}{70} & \frac{54}{7} & \frac{27}{35} & \frac{204}{35} & \frac{27}{40} & \frac{54}{35} & 0 \end{Vmatrix}$$

$$B' = \begin{Vmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \frac{1}{2} & \frac{1}{2} & 0 & 0 & 0 & 0 & 0 \\ \frac{1}{3} & \frac{4}{3} & \frac{1}{3} & 0 & 0 & 0 & 0 \\ \frac{3}{8} & \frac{9}{8} & \frac{9}{8} & \frac{3}{8} & 0 & 0 & 0 \\ \frac{14}{45} & \frac{64}{45} & \frac{8}{15} & \frac{64}{45} & \frac{14}{45} & 0 & 0 \\ \frac{95}{288} & \frac{125}{96} & \frac{125}{144} & \frac{125}{144} & \frac{125}{96} & \frac{95}{288} & 0 \\ \frac{41}{140} & \frac{54}{35} & \frac{27}{140} & \frac{68}{35} & \frac{27}{140} & \frac{54}{35} & \frac{41}{140} \end{Vmatrix} \quad (B)$$

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$$\bar{D} = \begin{vmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \frac{1}{12} & \frac{1}{12} & 0 & 0 & 0 & 0 & 0 \\ \frac{2}{15} & \frac{16}{15} & \frac{2}{15} & 0 & 0 & 0 & 0 \\ \frac{9}{40} & \frac{81}{40} & \frac{81}{40} & \frac{9}{40} & 0 & 0 & 0 \\ \frac{16}{63} & \frac{1024}{315} & \frac{144}{35} & \frac{1024}{315} & \frac{16}{63} & 0 & 0 \\ \frac{1375}{4032} & \frac{15}{448} & \frac{95}{2016} & \frac{95}{2016} & \frac{15}{448} & \frac{1375}{4032} & 0 \\ \frac{9}{25} & \frac{972}{175} & \frac{243}{35} & \frac{72}{7} & \frac{243}{35} & \frac{972}{175} & \frac{9}{25} \end{vmatrix}$$

(B) (Cont.)

$$\bar{D}' \begin{vmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \frac{1}{6} & \frac{1}{3} & 0 & 0 & 0 & 0 & 0 \\ \frac{4}{3} & \frac{2}{3} & 0 & 0 & 0 & 0 & 0 \\ \frac{3}{20} & \frac{27}{40} & \frac{27}{10} & \frac{39}{40} & 0 & 0 & 0 \\ \frac{64}{45} & \frac{16}{15} & \frac{64}{15} & \frac{56}{45} & 0 & 0 & 0 \\ \frac{275}{2016} & \frac{625}{1008} & \frac{3125}{1008} & \frac{625}{504} & \frac{11875}{2016} & \frac{1525}{1008} & 0 \\ \frac{54}{35} & \frac{27}{70} & \frac{204}{35} & \frac{27}{35} & \frac{54}{7} & \frac{123}{70} & 0 \end{vmatrix}$$

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When N is sufficiently large, the values of L_N and $\bar{L}_N$ vary little, which can serve as a criterion for selecting the number of iterations N.

The zero approximation for the turbulence factor and the step size h are selected. It is assumed for the first profile that k(z) is a linear function of height through the entire boundary layer

$$k(z) = \varkappa v_* z. \tag{47}$$

Then the following expression is obtained for β_j:

$$\beta_j = \frac{\varkappa^2}{m_0 \mathrm{Ro}^2} e^{\frac{\varkappa^2}{m_0 \mathrm{Ro}} jh}. \tag{48}$$

The Rossby parameter used in formula (48) is determined by using the exact solution of the equation of motion (17) with conditions (19) and (20), where the turbulence factor is computed by formula (47):

$$G(\eta) = 1 - u_0(\eta) - iv_0(\eta) = \frac{K_0\left(\frac{2}{\varkappa}\sqrt{m_0 i}\, e^{\frac{\varkappa^2}{2m_0 \mathrm{Ro}}\eta}\right)}{K_0\left(\frac{2}{\varkappa}\sqrt{m_0 i}\right)}, \tag{49}$$

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Starting with (49) and making use of K_0 for small values of the argument, the parameters Ro and m_0 are found to be connected by the formula

$$Ro \approx \frac{\sqrt{\frac{\pi^2}{4} + \left(2c + \ln \frac{m_0}{\pi^2}\right)^2}}{m_0}, \tag{50}$$

where c = 0.5772, the Euler constant.

When selecting the step size h, it is assumed that the correction for the Coriolis force is very small in the layer $0 \leq \eta \leq 6h$.

On the basis of (45)

$$\delta = \int_0^{6h} \beta(\xi)\,\xi\, d\xi, \tag{51}$$

where δ is a small number on the order of 10^{-2}—10^{-7}. Actual values of δ depend on the required accuracy. Using (51) and (48), the following transcendental equation is obtained for

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determining h:

$$e^{\frac{6\varkappa^2 h}{m_0 Ro}}\left[\frac{6\varkappa^2 h}{m_0 Ro} - 1\right] = \frac{\varkappa^2 \delta}{m_0} - 1. \qquad (52)$$

Thus, the order of computation is as follows:

1) The value of Ro is determined for the given value of the parameter m_0, then the step size h by (50);
2) The zero profile A_j is computed by formula (48);
3) The first seven values of A_j, A_j', etc., are computed by formulas (46);
4) The remaining values of A for j = 7, ..., N are determined by formula (43);
5) The values of speeds $u_0(\eta)$, $v_0(\eta)$, and their derivatives at all points η_j are computed by formulas (41), then the function $\varepsilon(\eta)$ by (33);
6) A new profile of the turbulence factor $\beta(\eta)$ is determined by formula (34). If $\beta(\eta)$ differs noticeably from its preceding value, all operations are repeated, starting with step 3).

When the first profile $\beta(\eta)$ is computed, the formulas given

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here can be used to determine other characteristics of the boundary layer as functions of the dimensionless height η.

Their dependence on the real height z can be determined by the formula

$$z = z_0 \left[1 + \mathrm{Ro} \int_0^{\eta} \beta(\eta) d\eta \right]. \qquad (53)$$

This method was tested on an M-20 computer for different values of the Rossby parameter; 5—7 approximations were required to achieve convergence of $\beta(\eta)$ with an accuracy of several percent (see Figs. 1 and 2). Orig. art. has: 2 figures, 52 formulas and 1 table. [W.A. No. 50; ATD Report 111]

SUB CODE: 04 / SUBM DATE: none / ORIG REF: 001 / OTH REF: 001

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0

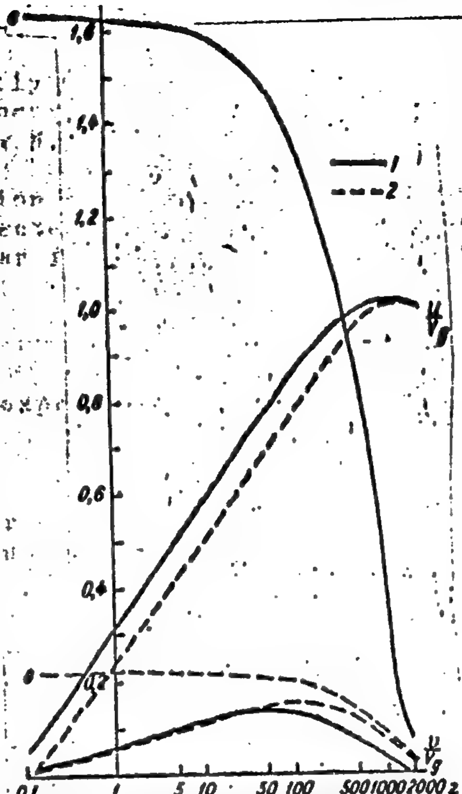

Fig. 1. Vertical profiles of the wind velocity components u/v_g, v/v_g, and turbulent energy $b(z)$.

1 - Log Ro = 6.1; 2- log Ro = 5.6

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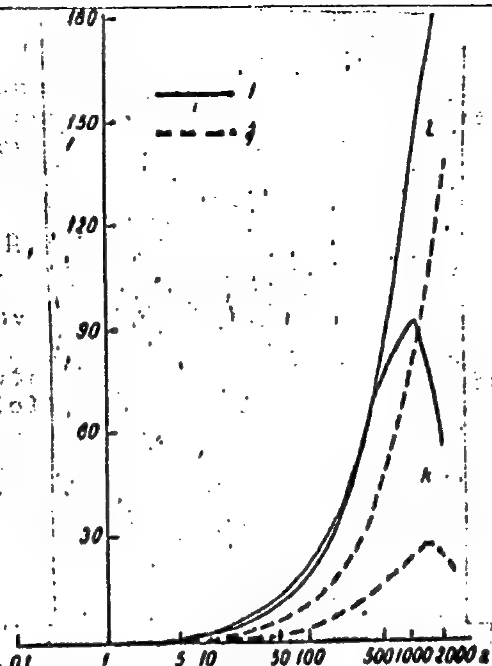

Fig. 2. Vertical profiles of the turbulence factor k(z) and the scale of turbulence l(z)
1 - Log Ro = 6.1; 2 - log Ro = 5.6.

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AP6032071 SOURCE CODE: UR/0362/66/002/009/0920/0927

AUTHOR: Vager, B. G.

ORG: Main Geophysical Observatory (Glavnaya geofizicheskaya observatoriya)

TITLE: Effect of turbulent diffusion in a semi-empirical model of the lower atmosphere

SOURCE: AN SSSR. Izvestiya. Fizika atmosfery i okeana, v. 2, no. 9, 1966, 920-927

TOPIC TAGS: lower atmosphere, atmospheric turbulence, atmospheric model, atmospheric diffusion, energy diffusion, turbulent energy

ABSTRACT: The author investigated a semi-emphirical model of turbulent transfer in the lower atmosphere proposed by S. S. Zilitinkevich and D. D. Laykhtman. A numerical solution of the problem is given, taking into consideration the effect of turbulent energy diffusion. It is shown that the effect plays an important role in unstable atmospheric stratification. The author thanks. S. S. Zilitinkevich for his help and valuable advice. Orig. art. has: 4 figures, 23 formulas and 1 table. [Based on author's abstract] SUB CODE: 04/SUBM DATE:22Apr66/ORIG REF: 009/ OTH REF: 001/ UDC: 551.551.8

Card 1/1

25(5) SOV/28-59-2-14/26

AUTHORS: Rabinovich, P.M., Khrisanfov, G.A.,(Moscow) Tager, L.A. (Moscow) and Shitikov, A.M.,(Leningrad); Engineers.

TITLE: On Revising Standards of the "Layout System" (K peresmotru standartov "Sistema chertezhnogo khozyaystva")

PERIODICAL: Standartizatsiya, 1959, Nr 2, pp 43-47 (USSR)

ABSTRACT: This article contains suggestions by four authors for layout standards now being revised. Different modifications to the preparation of working drawings, their registration and their storage, are proposed. There are 2 tables.

ASSOCIATION: TsNIITMASH; VNII.

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VAGER, R. M.

VAGER, R. M. -- "The Significance of 'Stolbur' and Fusarium in the Phenomenon of Premature Wilting of Potatoes in the South." Sub 9 May 52, Moscow Order of Lenin State U imeni M. V. Lomonosov. (Dissertation for the Degree of Candidate in Biological Sciences).

SO: Vechernaya Moskva January-December 1952

VAGER, R.M.

USSR/Agriculture - Plant Diseases

Mar/Apr 53

"Stolbur Wilting of Potatoes," R.M. Yager, Moscow Sta, All-Union Inst of Plant Protection

"Mikrobiologiya," Vol 22, No 2, pp 198-202.

Stolbur (caused by H. obsoletus) is entirely distinct from fusariosis and independent of secondary infection with the latter disease. In combatting potato wilting, ~~one must pay~~ primary attention to stolbur. In the ~~experiments~~ described, infection with H. obsoletus was carried out by using insects as transmitters or by applying ~~the method of grafting~~.

T3

VAGER, R.M.

Changes in the activity of respiratory enzymes of plants during virus infection. R. M. Vager (Plant Protection Sta., Moscow). *Zhur. Obshchei Biol.* 16, 298-305(1955).—Virus infection of whole plants or of isolated leaves of tobacco and tomato stimulated the activity of dehydrases, along with the activity of peroxidase. The activity of catalase in isolated leaves infected with virus, on the other hand, was decreased. No enzymic activity of the isolated and purified tobacco mosaic virus could be demonstrated. The increased enzymic activities in virus-infected plants is a result of a specific effect of the virus on the enzymes of the host plant.
J. A. Stekol

USSR/Virology - Plant Viruses. E.

Abs Jour : Ref Zhur - Biol., No 19, 1958, 85780

Author : Vager, R.M.
Inst :

Title : The Production of Specific Serum Against the Mosaic Virus of Winter Wheat.

Orig Pub : Dokl. VASKhNIL, 1957, No 12, 20-21

Abstract : Serum was prepared against the virus. The disease is transmitted by cicadas and is classified with the plant diseases known as the yellows. The total amount of injected antigen comprised 69.6 mg in doses of 2.5 to 6 ml of liquid. The serum produced a reaction only with the juice of sick plants in a dilution of 1:8.

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KONAREV, Vasiliy Grigor'yevich, prof.; VAGER, R.M., red.; PARSADANOVA, K.G., red.izd-va; VORONINA, R.K., tekhn.red.

[Nucleic acids and morphogenesis of plants] Nukleinovye kisloty i morfogenez rastenii. Moskva, Gos.izd-vo "Vysshaia shkola," 1959. 346 p. (MIRA 13:6)
(Nucleic acids) (Plants--Metabolism) (Morphogenesis)

VAGER, R.M.; KARPENKO, G.A.

Chemical structure of the mosaic virus of winter wheat. Vop. virus 7 no.4:106-109 Jl-Ag '62. (MIRA 15:8)

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Using ultraviolet spectrophotometry for the diagnosis of virus diseases in plants. Vop. virus. 8 no.1:91-94 Ja-F'63. (MIRA 16:6)

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(VIRUS DISEASES OF PLANTS) (SPECTROPHOTOMETRY)
(ULTRAVIOLET RAYS)

[illegible]

22013 Yager, V.[illegible] Ob organizatsii [illegible] obsluzhivaniya [illegible] vrachei. [illegible], [illegible] 24, 194[illegible], s. [illegible].

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36386 Nekotoryye pokazateli raboty poliklinik, ob"Yedinennykh S Bol'nitsami. Sov. Vracheb. Sbornik. Vyp. 16, 1949, S. 29-31

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(CARDIOVASCULAR SYSTEM—DISEASES)
(DISAVILITY EVALUATION)

KOMOR, Karoly, dr.; SZECSENYI, Nagy L.,dr.; VAGFALVY, Ilona, dr.

Differentiation of hypophysial and thyreogenic myxedema by radioiodine on the basis of the thyrotropin test. Magy.belorv. arch. 13 no.4:110-112 Ag '60.

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(MYXEDEMA diag)
(PITUITARY GLAND dis)
(THYROTROPIN pharmacol)
(IODINE radioactive)

VAGEROV, V.S.; FARTUKOV, M.M.; CHIRVA, G.I.; SHCHAVELEVA, A.P.

Upper Cretaceous sediments of the Bakhardoksk keyhole. Izv. AN Turk.SSR.Ser.fiz.-tekh., khim. i geol.nauk no.5:49-54 '65. (MIRA 18:11)

1. TSentral'naya kompleksnaya tematicheskaya ekspeditsiya GPGK Turkmenskoy SSR.

KOMOR, Karoly, dr.; SZECSENYI, Nagy Laszlo, dr.; MAGFALVY, Ilona, dr.

Basal metabolism tests following chlorpromazine injections and determination of the I-131 curves in thyroid function tests. Magy. Belorv. arch. 15 no.2:70-73 Ap '62.

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(CHLORPROMAZINE pharmacol) (THYROID GLAND pharmacol)
(BASAL METABOLISM pharmacol) (IODINE radioactive)

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V[illegible], J.

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The Gyor 2 performance glider. p. (3) of cover.
PAI-6, a Soviet glider. p. (3) of cover. [illegible]. Budapest. Vol. 9, No. 1, Jan. 1956

SOURCE: East European Accessions List (EEAL) Library of Congress
Vol. 5, No. 6, June 1956

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VAGHY, Antal

Verification of the Diesel metering jet test bench. Auto motor 13 no.21:13 1 N '60.

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VAGHY, Tamas, [illegible] University, Department of ~~Surgery and~~ Ophthalmology, [illegible] KOVACS, Andras, Dr, professor, cand. of vet. sci.) ([illegible] Egyetem, Sebeszeti es Szemeszeti Tanszeke es Klinikaja).

"Experimental [illegible]."

Budapest, [illegible] Feb 6[illegible], pages 66-69.

Abstract: [Authors' English summary modified] The bactericidal effect of a weak aqueous solution of phenyl-[illegible] ($C_6H_5HgBO_2$) - phenomerforum [illegible] with special emphasis on the [illegible] by the 0.2 per cent [illegible] of Fimos[illegible], even in a 10-20-fold dilution. [illegible] not observed and the solution was harmless to the tissues [illegible] in contact with it. When larger quantities were introduced, however (i.e. for rinsing the abdominal cavity) Hg poisoning developed. Following i.v. administration, the experimental animals [illegible] the solution [illegible] purulent [illegible] and [illegible] before reposition. [illegible]

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Budapest, Hungary

So: East European Accession, Vol. 5, No. 5, May 1956

HUNGARY

FELKAI, Ferenc, Dr., and VAGHY, Tamas, Dr., Assistant Professors, Chair and Clinic for Surgery and Ophthalmology at the University for Veternary Sciences (Allatorvostudomanyi Egyetem Sebeszeti es Szemeszeti Tanszeke es Klinikaja)[location not given](Head: KOVACS, Andras B., Dr., Professor, Candidate of Veterinary Sciences).

"Some Instances of the Application of Trypsin Wound Powder"

Budapest, Magyar Allatorvosok Lapja, Vol 21, No 5, May 1966, pp 231-235.

Abstract: Twenty-six cases illustrating the uses of Trypsin wound powder, containing 0.25 g. trypsin, local anesthetic, stabilizer, and glycocoll in 10-g. shaker-type jars, were described. The experiences were generally favorable, confirming reports in the literature regarding the performance of trypsin-containing wound powders. It was especially effective in the treatment of abscesses and fistulas. No allergenic reactions were noted. The powder should be administered every 6-8 hours for about 2-3 days. It does not serve as a substitute for medical or surgical procedures, but it supplements them. 29 references, including 8 Hungarian, 4 German, and 17 Western.

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HUNGARY

VASHY, Tamas, Dr, MESZAROS, Janos, Dr; Veterinary Medical University, Department of Surgery and Ophthalmology, and Clinic (chairman: B., KOVACS, Andras, Dr, professor, cand. of vet. sci.) and Department of Pathological Anatomy (chairman: KARDEVAN, Andor, Dr, docent) (Allatorvostudomanyi Egyetem, Sebeszeti es Szemeszeti Tanszek es Klinika, es Korbonctani Tanszek).

"Intermittent Lameness in a Horse Caused by Thrombosis."

Budapest, Magyar Allatorvosok Lapja, Vol 21, No 10, Oct 66, pages 461-463.

Abstract: [Authors' English summary modified] On the basis of the clinical symptoms and of the results of rectal and other complementary examinations (pCO_2determination of the venous blood), the presence of a thrombi was diagnosed in the quadrifurcation of the aorta as well as in the pelvic and iliac arteries. The animal received no treatment because of the poor prognosis. In the course of dissection of the animal, large white and mixed thrombi were found in the above mentioned vessels which filled up the lumen to about three-fourth of its volume. It is suggested by the authors that the pathological process originated most probably from an unknown injury to the intima. The post mortem examination revealed that the development of the thrombosis was started in the right iliac artery. Chondrous islands originating from metaplasia were also found at several places of the organized areas. 8 Hungarian, 15 Western references.

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"Economy in Road Planning; Remarks on Istvan Czuni's Study", P. 104, (KOZLEKEDESTUDOMANYI SZEMLE, Vol. 4, No. 3, Mar. 1954, Budapest, Hungary)

SO: Monthly List of East European Accessions, (EEAL), LC, Vol. 3, No. 12, Dec. 1954, Uncl.

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Melyepitestudomanyi Szemle. - Vol. 4, no. 12, Dec. 1954.

Rounding off longitudinal sections and building superelevated crossings on public roads. p. 649.

SO: Monthly list of East European Accessions, (EEAL), LC, Vol. 4, No. 9, Sept. 1955 Uncl.

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Temporary roads to construction sites. p. 543.
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